

# Comparison of PV Module Performance Before and After 11, 20, and 25.5 Years of Field Exposure

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**Abstract** — In 1990, 192 ARCO M75 photovoltaic (PV) modules were installed at the HSU Telonicher Marine Lab in Trinidad, California, 150 meters inland from the Pacific Ocean. Current-voltage (IV) tests were performed on each module prior to the array's construction in 1990 [1] and then again in 2001 [2], 2010 [3], and most recently in 2016 after the array was decommissioned. After 25.5 years, 188 of the original 192 modules remained operational. Over their lifetime, the modules' maximum power at the normal operating cell temperature (NOCT) declined by an average 21.6% with a degradation rate of 0.85% per year. The average degradation rate grew from 0.4%/year in the first 11 years to 0.81%/year after 20 years to 0.85%/year after the total 25.5 years.

## I. INTRODUCTION

### A. Background

The Schatz Solar Hydrogen Project, directed by the Schatz Energy Research Center, was installed in 1990 at the HSU Telonicher Marine Laboratory in the coastal California town of Trinidad. The project's objective was to demonstrate the use of hydrogen to store energy from a renewable energy power system. The system powered the Marine Laboratory aquaria air-compressor either directly from the 9.2 kW-rated solar PV array (with an azimuth of due south and a tilt of 28°) or indirectly using a hydrogen-fueled proton exchange membrane (PEM) fuel cell. The hydrogen for the fuel cell was generated by a Teledyne Energy ALTUS 20 electrolyzer powered by the PV array.

The solar array (see Fig. 1) offered the unique opportunity to measure the performance degradation of the individual modules over 25.5 years of field exposure. Data from this analysis can be used to track the causes of module failures, degradation in power output, and help characterize a timeline of expected performance of such mono-crystalline silicon PV modules. When new, these ARCO M75 modules were rated by the manufacturer at 48 W at standard testing conditions (STC or 1000 W/m<sup>2</sup> at a module temperature of 25°C), which is equivalent to 46.4 W at NOCT (defined here as 1000 W/m<sup>2</sup> at 47°C). Each module is glazed with tempered glass and ethylene vinyl acetate (EVA) encapsulant and contains 33 cells in series with two bypass diodes per module. The lasting effect of the bypass diodes is also analyzed later in this study.

Zoellick [1] set the precedent for the three successive testing cycles. He used a capacitive-based curve tracer connected to a

computer interactive data acquisition system to test and record IV curves for each module using methods approved by the American Society of Testing and Materials (ASTM).



Fig. 1. A view of the array during decommissioning after two subarrays had already been removed (Photo Credit: Mark Rocheleau)

### B. Previous Findings

Zoellick [1] found in his 1990 testing that the average maximum power ( $P_{\max}$ ) was 39.88 W and the average short circuit current ( $I_{sc}$ ) was 3.29 A, about 10% lower than the manufacturer advertised specifications. Thereafter, Zoellick's results were used as the base case data for the following rounds of testing in 2001, 2010, and 2016. The 2001 cycle of tests [2] found that the average  $P_{\max}$  and  $I_{sc}$  had dropped to 38.13 W and 3.15 A, respectively, representing a 4.40% decline over 11 years of operation.

The 2010 tests, after 20 years of field exposure, reported larger degradation for both parameters. The  $P_{\max}$  experienced a 12.3% decrease from the 2001 testing to 33.43 W, bringing the total loss to 16.1% from the 1990 tests, and the  $I_{sc}$  dropped 6.04%, down to 2.96 A, in the second decade for a total lifetime decline of 10.2%. For the maximum power, the average degradation rate over the 20-year interval came to 0.81%/year, but the degradation rate over the second decade (2001-2010) was 1.4%/year, more than three times the degradation rate over the first decade of 0.4%/year. This suggests that the performance of the modules degraded more rapidly as they aged, instead of following the expected pattern of linear degradation.

Other IV curve parameters also changed over the first two decades of operation (Fig. 2). The series resistance ( $R_s$ ), parallel resistance ( $R_p$ ), and the “ekt” variable (which controls the degree of curvature near the maximum power point) all experienced dramatic variations as evidenced by changes in the slopes and curves of the IV curves. After only 11 years, the average  $R_p$  had dropped by 33.75%, the average  $R_s$  had increased by 10.66%, and the average ekt rose by 26.38%. The inverse of  $R_p$  is the slope of the IV curve as the voltage approaches zero, and the negative inverse of  $R_s$  is the slope of the IV curve as the current approaches zero. In contrast, the average open circuit voltage ( $V_{oc}$ ) hardly changed, falling by only 1.0%, or 0.17 V, over 20 years.

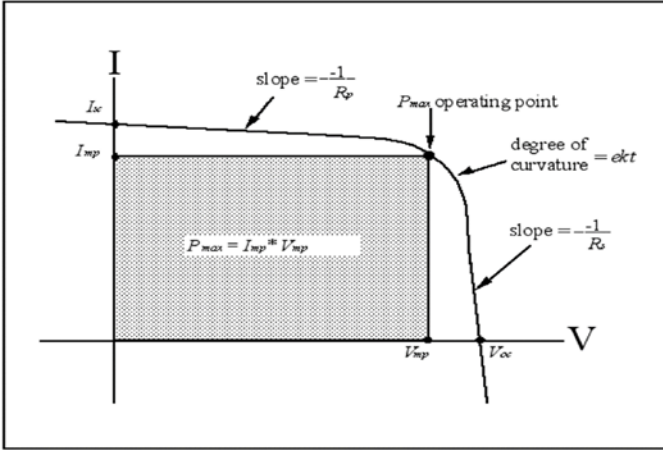


Fig. 2. Five-parameter IV curve showing the location of the maximum power point on the curve [2]

## II. PROCEDURE

### A. Testing

The conditions in which Zoellick [1] performed his tests were replicated as closely as possible in all subsequent rounds of testing in 2001, 2010, and 2016. Each module was tested outside at a module temperatures centered around 47°C with tests ranging from 25-65°C, a solar insolation of at least 800 W/m<sup>2</sup> (but closer to 1000 W/m<sup>2</sup> when achievable), and an air-mass (AM) less than or equal to 1.5. Each module was cleaned prior to testing, eliminating any dust or dirt that would prevent the module from generating at its optimum level for the analysis.

The 1990 and 2016 rounds of testing used a portable and adjustable frame to test each module, but in the 2001 and 2010 testing the array still in operation so each module was tested within the plane of the array. An Eppley PSP pyranometer and a surface mount type-T thermocouple were used to monitor and record the solar insolation in the plane of the module and the module temperature, respectively.

While the different rounds of testing used slightly different methods and technologies to produce IV curves, each one used a capacitive load and was completed in 10 seconds or less.

The 2016 testing used a Mini-KLA PV IV Curve Tracer [4] and its associated MiniLes (R) program to measure and record the pertinent current and voltage data (Fig. 3). This instrument reported the observed  $P_{max}$ ,  $V_{oc}$ ,  $I_{sc}$ , maximum power voltage ( $V_{mp}$ ), maximum power current ( $I_{mp}$ ), the IV curve fill factor (FF), and a plot of the IV curve on its graphical interface. The insolation was measured using an Eppley PSP pyranometer and the module temperature was measured using a type-T surface mount, quick response thermocouple positioned in the center of the back of the module.

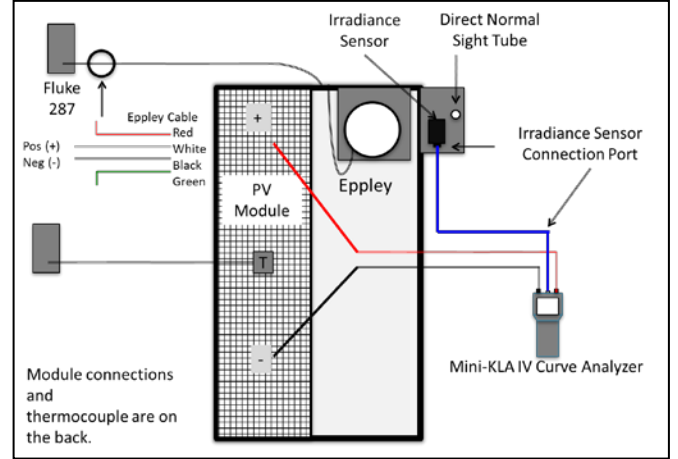


Fig. 3. Schematic showing the 2016 testing apparatus and third party measurement instruments (by Jake Rada)

### B. Data collection and standardization

Zoellick [1] adjusted all observations to NOCT conditions based on the observed sensitivity of the module  $V_{oc}$  to insolation and module temperature. His and all subsequent corrections adjusted  $V_{oc}$  with respect to the measured module temperature (-0.0603 V/°C) and insolation (0.0009296 V\*m<sup>2</sup>/W). Based on a Schottky diode model, these analyses fit the module IV curve to a parameter model, where:

$$I = I_L - \frac{I_L - V_{oc}}{R_p} \left\{ \frac{\exp[ekt(V + R_s I)]}{\exp[ektV_{oc}] - 1} - 1 \right\} - \frac{(V + R_s I)}{R_p} \quad (1)$$

where:

- ekt = q/(nkT) [V<sup>-1</sup>]
- I = module current; initial guess [A]
- V = module voltage [V]
- I<sub>L</sub> = light induced module current [A]
- V<sub>oc</sub> = open circuit module voltage [V]
- R<sub>s</sub> = module series resistance [Ω]
- R<sub>p</sub> = module parallel resistance [Ω]
- q = electronic charge [coulomb]
- n = ideality factor per cell [unitless]
- k = Boltzmann's constant [Joule/K]
- T = temperature [K]

In 2016 testing, the Eppley PSP pyranometer and thermocouple readings were recorded by hand. The MiniLes software takes the data from the Mini-KLA and converts it into a text file. Then software written in Sci-Lab [5], modified from that previously used in the 2010 testing analysis filtered the readings, standardized the data to 1000 W/m<sup>2</sup> and 47°C using the correction factors from Zoellick and used nonlinear regression to estimate the parameters of Equation 1.

### III. RESULTS AND DISCUSSION

After 25.5 years, every single module from this array is discolored and shows signs of delamination. Signs of hot spots with a range of severity have become common in the modules. Fig. 4 shows a comparison between one of the most physically degraded ARCO M75 modules and one of the younger replacement Siemens SM50-H modules. The ARCO module has been exposed to the environment for 26 years old in this image, and the Siemens module has been in the field for 19 years; note the obvious anti-aging improvements in the newer model. This study goes on to investigate whether the increased prevalence of physical degradation led to larger power losses in these modules over the project lifetime.



Fig. 4. A physical comparison between a 26-year old ARCO M75 module and a 19-year old Siemens SM50-H (Photos by Jake Rada)

Fig. 5 compares the distributions of the P<sub>max</sub> of the modules from each testing cycle (i.e., 1990, 2001, 2010, and 2016) in a normal probability plot. The initial 1990 curve remains close to linear throughout the curve, and as the modules aged the standard deviation of the P<sub>max</sub> among the modules increased. This is exemplified by the steeper slopes and wider P<sub>max</sub> ranges in the later years that include modules that have lost

significant power. In the 2016 testing cycle, two modules had their P<sub>mas</sub> drop below 10 W.

Fig. 6 shows the average P<sub>max</sub> of all the modules for each testing cycle and notates the modules' age during testing. There is clearly less linear degradation from 1990-2001 followed by a steeper degradation from 2001 to the end of the project. The degradation rates (i.e. rates of power loss) for the testing windows include 0.4%/year for the first 11 years (1990-2001), 1.4%/year for the next nine years (2001-2010), and 1.3%/year for the last five and a half years of the project (2010-2016). The average lifetime degradation rate of the 25.5-year project came to 0.85%/year. Fig. 3 has a linear trend line whose equation says that roughly 0.35 W were lost each year for the modules, which, based on the original 1990 average of 39.88 W, is just over 0.85%/year of power loss.

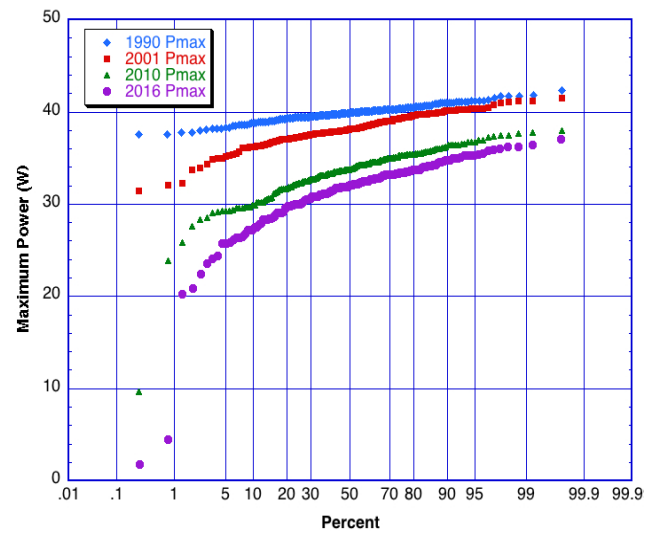


Fig. 5. P<sub>max</sub> distribution curve for all modules in four test cycles

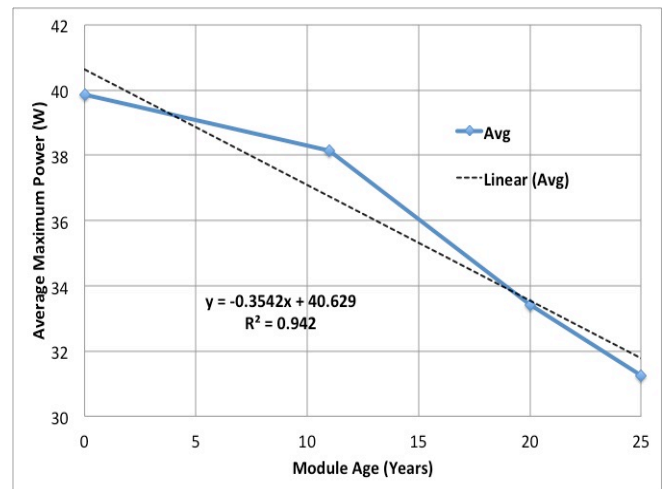


Fig. 6. Average P<sub>max</sub> based on the age of modules during testing



Each module incorporated two bypass diodes to avoid the creation of localized hot spots, as they direct the current around cells that are either damaged or shaded. The associated effect of the action of the diodes is to reduce the module  $P_{max}$ . Fig. 7 shows the IV curves from 1990, 2001, 2010, and 2016 for a single module that lost a small amount of its  $P_{max}$  in the first decade of operation but then saw a significant loss in the second decade of field exposure. This second “knee” in the IV curve is a result of the bypass diode directing the current around 22 of the 33 cells in the module. These second knees were uncommon in the 2001 testing, but in the 2016 testing all but 13 of the modules had significant second knees. The fifth curve in this figure shows the effect of removing these bypass diodes from a module with a significant second knee. Results show that this action increases the  $P_{max}$ , but the potential for exacerbating hot spots may increase.

Bypass diodes were removed from several modules in 2016 and then retested. Fig. 7 shows the most extreme change caused in the IV curve through this removal of bypass diodes, but this dramatic change to the IV curve only resulted in an increase in the module’s  $P_{max}$  by 1.3 W, or less than a 5% increase in power generation. This analysis showed that the bypass diodes provided significant over-current protection for the sacrifice of less than 5% of their power generating abilities on average. Modules that did not experience second knees in their IV curves were hardly affected when tested with or without their bypass diodes as the diodes had not be routinely or permanently activated to redirect current around problematic cells, which leads to less cells generating power.

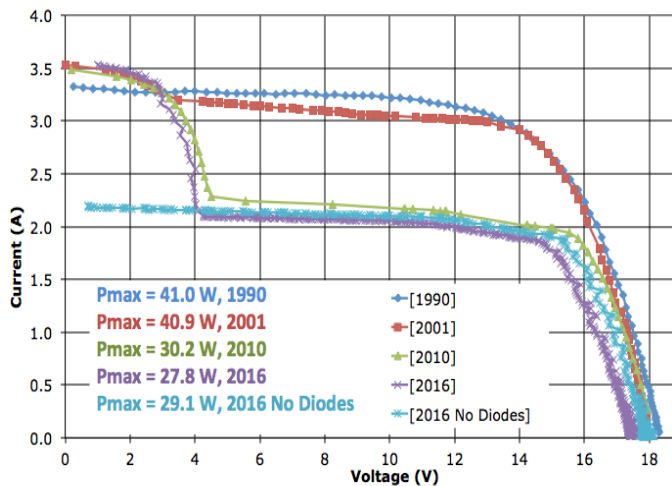


Fig. 7. IV curve for a module that shows the effect of diodes

#### IV. CONCLUSION

After 25.5 years, almost 16 years after the modules’ 10-year warranties expired, the modules averaged a power loss of 21.6% from their initially tested power outputs for an average degradation rate of 0.85%/year. The average standard deviation of the power output also increased from 0.92 W to 4.10 W during this time. This calculated degradation rate is only slight higher than the expected range of 0.5-0.8%/year [6]. The 2016 testing supports past analyses conclusions identifying the drop in  $I_{sc}$  as the primary source of power loss, which can be attributed to the increased presence of EVA browning, physical delamination, and localized hot spots with the modules. Future studies may have the opportunity to assess to what degree the degradation of the crystalline cells and the EVA encapsulant have on this measured drop in  $I_{sc}$  that contributed most heavily to the power loss in these modules.

In 2016 almost half (48%) of the remaining original 188 ARCO M75 modules still generated 80% or more of their initial capabilities tested in 1990, and 90% of them still generate over 70% of their initial power measurements. As one of the oldest, if not the oldest, and best monitored PV arrays of its kind, the results from this 26-year long project can be greatly beneficial to the solar energy industry, as bankability and longevity dictate the successful marketing of this energy generation technology.

#### REFERENCES

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